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Research Article

# The Kinetic Modeling of Methane Hydrate Growth by Differential Scanning Calorimetry Measurements and Molecular Dynamic Simulations

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# ARTICLE INFO

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#### **ABSTRACT**

The formation kinetics of methane hydrate were examined using differential scanning calorimetry (DSC) and molecular dynamics (MD) simulations. A kinetic model was established based on principles of irreversible and non-equilibrium thermodynamics and the concept of the thermodynamic natural path. This model employed affinity as a thermodynamic function, driving the hydrate formation process. It accurately predicted methane hydrate growth from both experimental and simulation data, demonstrating that hydrate formation follows a natural path. This model includes two parameters with distinct dependencies. One parameter, n, remained nearly constant, with experimental results averaging -6.8 and simulation data ranging from -1.05 to 1.46. The other parameter, k, is influenced by operational conditions and serves as a kinetic index. The value of k changed with variations in temperature, pressure, and additive concentration, increasing by 10 to 100 times with higher system pressure and by 2 to 3 orders of magnitude with the addition of tetrahydrofuran.

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# 1. Introduction

Gas hydrates are crystalline solids formed by trapping small gas molecules, like methane, or polar molecules, such as tetrahydrofuran (THF), within water cavities made of hydrogen-bonded water molecules [1,2]. Methane hydrate reservoirs on the deep ocean floor are estimated to contain about 6.4 trillion tonnes of methane [3], representing a significant potential energy resource. However, these hydrates can pose challenges for the petroleum

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industry by clogging gas pipelines. Therefore, improving our understanding of these compounds could offer new insights into previous experimental and theoretical data.

Research has focused on understanding the fundamental mechanisms of nucleation, growth, and dissociation of gas hydrates. Ongoing studies continue to explore these processes due to their relevance in methane hydrate exploration and exploitation [4-8]. Prof. Bishnoi's group, with a long history in the Western Hemisphere, has been at the forefront of macroscopic kinetics studies of hydrate growth and decomposition since the early 1990s, pioneering kinetic modeling of gas hydrates [9-11]. Since then, research has increasingly addressed macroscopic, mesoscopic, and molecular scale time-dependent measurements. Over the past two decades, advanced experimental and modeling techniques have been employed to tackle these measurements.

Differential scanning calorimetry (DSC) is one of the most widely used methods for measuring the thermal properties associated with gas hydrate formation and dissociation [12,13]. Researchers such as McNamee and Dalmazzone et al. have demonstrated that DSC can be an effective tool for evaluating hydrate formation kinetics [14,15]. For instance, Dalmazzone et al. utilized DSC data to develop a model based on crystal growth theory, which illustrates the hydrate formation rate over time [16].

In addition to macroscopic measurements and kinetic modeling, understanding the molecular mechanisms of hydrate formation is crucial for explaining its various properties. Molecular dynamics (MD) simulations are a powerful tool for elucidating crystal growth mechanisms [17-22]. Nada explained that gas hydrate growth involves transferring gas molecules from the gas phase through the liquid phase to the liquid/clathrate interface, followed by the organization of water molecules around the gas molecules at the interface [23]. These stages are key factors in the hydrate growth rate and should be incorporated into kinetic models. Several kinetic models of gas hydrate formation and decomposition have been based on molecular simulation data. For example, Tung et al. developed a simple adsorption-diffusion model to predict methane hydrate growth by considering methane mass transport in the bulk phase and its adsorption by water cages in the growing layer [24].

This work aims to provide a straightforward and practical approach for studying methane hydrate growth kinetics at both macroscopic and molecular levels. We utilized high-pressure DSC and molecular dynamics simulations to gather data on methane hydrate growth kinetics and applied a model grounded in non-equilibrium thermodynamics and the concept of the thermodynamic natural path for kinetic modeling.

## 2. Methods

# 2.1. Experimental

To prepare the solution, freshly deionized and distilled water, sodium dodecyl sulfate (SDS), and tetrahydrofuran (THF) with a purity of 99.5% from Merck were used. The experiments were carried out using a high-pressure differential scanning calorimeter (DSC) equipped with two cylindrical stainless-steel cells, each with an outer diameter of 0.4 cm, a length of 9 cm, and an internal volume of approximately 1.1 cm<sup>3</sup>. A copper segment, comprising three rectangular cubic sub-segments, was designed to hold the cells, two platinum thermometers (Pt100), and peltiers (4 cm  $\times$  4 cm) for cooling and heating. The cells, which could withstand a maximum pressure of 20 MPa with a deviation of  $\pm$ 0.05 MPa, were positioned in the central segment. Each cell was equipped with thermometers placed underneath, offering accuracy of  $\pm$ 0.1 °C and precision of  $\pm$ 0.01 °C. The peltiers managed the temperature control, with refrigerant fluid circulating through the surrounding copper segments to cool the hot surfaces. The copper segment and its components were housed in an insulated plexiglass

chamber, with temperature regulation provided by a programmable controller. A schematic of the experimental setup is illustrated in Fig. 1.

For the testing procedure, a sample of  $0.25 \pm 0.025$  cc of the solution was injected into a pre-evacuated cell. The gas pressure was then adjusted and maintained at a constant level throughout the process. Both the sample and an empty reference cell were placed in the respective cavities of the central copper segment. The temperature was ramped down from 15 to -15 °C at a rate of 0.5 °C/min. Each experiment was performed two or three times to ensure repeatability.

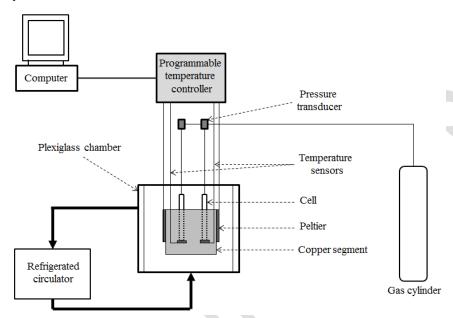


Fig. 1. Schematic diagram of the experimental apparatus of DSC.

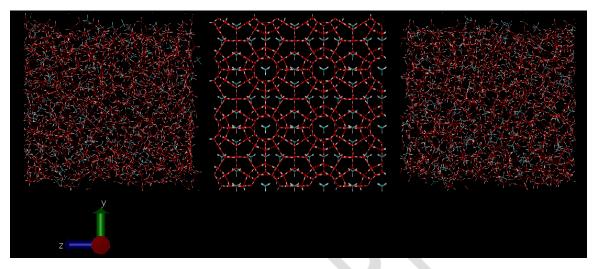
#### 2.2. Simulation details

All molecular dynamics simulations were conducted using the open-source software package LAMMPS [25]. The initial configuration of the simulation box, measuring  $36 \text{ Å} \times 36 \text{ Å} \times 110 \text{ Å}$ , is illustrated in Fig. 2. This setup included a  $3 \times 3 \times 3$  unit cell of structure I methane hydrate phase, flanked by two methane/water aqueous solutions. Each hydrate cavity was fully occupied by methane molecules, and each solution slab contained 1242 water molecules along with 25, 50, or 75 methane molecules, making them supersaturated methane/water solutions.

To model the intermolecular interactions of water and methane molecules, the SPC and OPLS-AA potentials were utilized, respectively [26,27]. The SHAKE algorithm was applied to constrain the bond lengths and angles of water molecules [28]. For cross-LJ parameters ( $\varepsilon$ ,  $\sigma$ ) between water and methane molecules, the standard Lorentz-Berthelot combining rules were used [29]. Long-range electrostatic interactions were computed using the Ewald method [30] with a precision of  $1\times10^{-4}$  (k-space cutoff), and all intermolecular interactions were truncated at a spherical cutoff of 11.0 Å. The force field parameters employed in the simulations are detailed in Table 1.

The equations of motion were integrated using the Verlet algorithm with a time step of 1 fs. The simulation was executed in three stages: (1) the water/methane solution phases were equilibrated using the NPT ensemble for 100 ps while keeping the hydrate phase frozen, (2) a brief 35 ps simulation was then conducted to thermalize the clathrate hydrate molecules and relieve any residual stress in the system, and (3) the simulation continued for a

total duration of 10 ns under NPT conditions. The temperature was maintained between 240-270 K and the pressure between 5-25 MPa using the Nose-Hoover barostat and thermostat [31], respectively. Periodic boundary conditions (PBCs) were enforced in all directions, effectively simulating an infinite system by replicating the main cell to eliminate boundary effects, albeit with potential periodicity artifacts.



**Fig. 2**. The initial setup of the simulation system. Cyan, red, white spheres indicate C, O and H atoms, respectively.

**Table 1**. Force field parameters for water and methane [26,27].

Interaction		σ(Å)	ε (kcal/mol)	q (electrons)
H <sub>2</sub> O	O	3.166	0.1553	-0.820
	H	0	0	0.410
		r(OH) = 1.00  Å	$\theta(\text{H-O-H}) = 109.47^{\circ}$	
CH <sub>4</sub>	C	3.500	0.0660	-0.240
	H	2.500	0.0300	0.060
		r(CH) = 1.09  Å	$\theta(H-C-H) = 107.80^{\circ}$	

## 2.3. Kinetic modeling

A kinetic model was formulated to predict hydrate growth kinetics using irreversible and non-equilibrium thermodynamics along with the concept of the thermodynamic natural path [32]. When a chemical process like hydrate formation occurs in an isolated system by an amount of  $d\xi$  over an infinitesimal time interval, it generates an amount of uncompensated heat, diQ, and thus creates an amount of entropy, diS. Based on this, De Donder's inequality was introduced, utilizing a new energy function termed affinity, A, for irreversible processes [33], as follows:

$$d_i Q = T d_i S = A d\xi) 0 \tag{1}$$

This affinity equation connects the entropy generated from uncompensated heat to the irreversible chemical process occurring in nature. A positive affinity (A>0) indicates that the irreversible reaction is proceeding, while A=0 signifies that the process has reached equilibrium. Consequently, the affinity decreases as the irreversible process continues, making affinity the driving force for such processes. The rate of entropy increase or heat loss can be derived from Eq. (1):

$$\frac{d_i Q}{dt} = T \frac{d_i S}{dt} = A \frac{d\xi}{dt}$$
(2)

The thermodynamic flow,  $d\xi/dt$ , can be considered the velocity of the process or the rate of conversion, as shown below:

$$r = \frac{d\xi}{dt} = kA^n \tag{3}$$

Therefore, Eq. (2) can be rewritten as:

$$\frac{d_i Q}{dt} = T \frac{d_i S}{dt} = A \frac{d\xi}{dt} = kA^{n+1} > 0 \tag{4}$$

According to Eq. (4), the rate of creation of uncompensated heat and entropy production is proportional to the (n+1)-th power of the driving force, A. This model requires two parameters, k and n, for the kinetic modeling of the gas hydrate formation process.

#### 3. Results and discussion

# 3.1. Methane hydrate growth from DSC measurements

Fig. 3 displays a DSC thermogram illustrating CH<sub>4</sub> hydrate and ice formation at a pressure of 5.2 MPa. The initial peak corresponds to CH<sub>4</sub> hydrate formation, as indicated by a significant pressure drop at around 5.5°C. The subsequent peak, near -14°C, is associated with ice formation from un-hydrated water and was excluded from further analysis.

From the right side of Fig. 3, it is evident that once hydrate formation occurs, the heat of formation is released, causing a sudden increase in heat flow to a certain value (marked as "A" in Fig. 3). Region A signifies the rapid initial growth phase where water molecules convert to gas hydrates, releasing substantial methane hydrate formation heat. When the hydrate formation rate equals that of the cooling system, the heat flow stabilizes at the peak, indicating a metastable state. This is because the heat generated by hydrate formation is not significantly higher than the cooling capacity, leading to a gradual decrease in heat flow until it returns to baseline (marked as "B" in Fig. 3). Thus, the initial step of the process (Region A) can control gas hydrate growth and is evaluated in this study.

Fig. 4 shows the heat flow over time for CH<sub>4</sub> hydrate formation in an SDS aqueous solution with and without THF at system pressures ranging from 4.9 to 5.5 MPa. A small amount of SDS, an anionic surfactant, was added to enhance the gas/solution interface and improve CH<sub>4</sub> diffusion into the solution. As seen in Fig. 4, both the heat flow rate and peak height increase with rising pressure. Higher pressure results in more nucleation sites with faster kinetics, accelerating growth [2]. The presence of THF also boosts the heat flow rate and peak height. Literature confirms that THF promotes gas hydrates by altering the clathrate hydrate structure [34-38]. Zhang et al. noted that adding 6 mol% THF to water significantly lowers CH<sub>4</sub> hydrate formation pressure by forming structure II hydrate [36]. Raman measurements revealed that CH<sub>4</sub> molecules are trapped in the small 512 cages of sII hydrate formed by THF, while the larger 51264 cages are mostly occupied by THF molecules [37]. This additive shifts the hydrate phase boundary to lower pressures and higher temperatures, increasing the driving force for hydrate nucleation [38]. Consequently, THF is recognized as an effective promoter of gas hydrate formation kinetics.

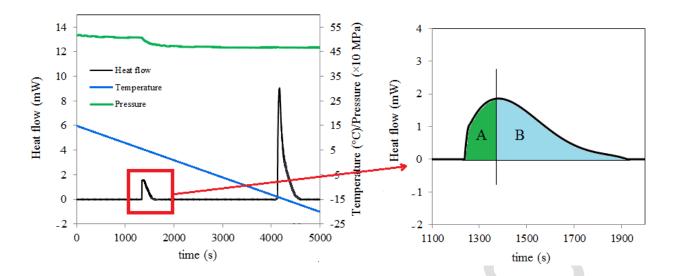


Fig. 3. DSC curve of CH<sub>4</sub> hydrate formation at 5.2 MPa.

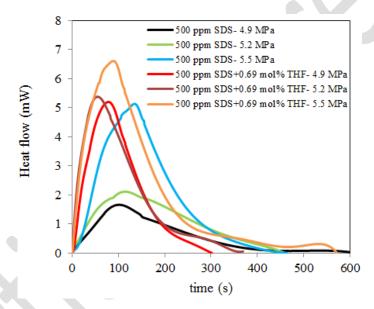


Fig. 4. DSC curve of CH<sub>4</sub> hydrate formation at different pressures in the presence of SDS and THF.

To determine the model parameters k and n from Eq. (3), the extent of the process  $\xi$  and the affinity A must be calculated. The extent of the process can be found by dividing the peak area of the heat flow versus time into infinitesimal segments and then calculating the ratio of the accumulated area over time to the total peak area. Fig. 5 shows the extent of the process over time for CH<sub>4</sub> hydrate formation, displaying an S-shaped curve similar to a sigmoid growth pattern [39]. The initial portion of hydrate formation corresponds to an exponential growth rate, as illustrated in Fig. 5. Once the extent of the process is calculated, the affinity can be determined using Eq. (4):

$$A = \frac{\frac{d_i Q}{dt}}{\frac{d\xi}{dt}}$$
 (5)

Fig. 5 also illustrates the affinity over time for CH<sub>4</sub> hydrate formation at 5.2 MPa. The affinity of hydrate formation is positive (A>0) before equilibrium and zero (A=0) at equilibrium. As the process moves towards equilibrium, the

affinity decreases towards zero, indicating the decay path of the affinity. Initially, at the beginning of CH<sub>4</sub> hydrate formation, the affinity is very high but decreases as the process progresses, stabilizing at a constant value corresponding to the peak of heat flow. Subsequently, the affinity decreases further until it reaches zero. This behavior suggests that as more hydrate forms, the diffusion of CH<sub>4</sub> into the aqueous phase decreases and the CH<sub>4</sub>/solution interface becomes covered by the solid hydrate phase, which slows down the affinity.

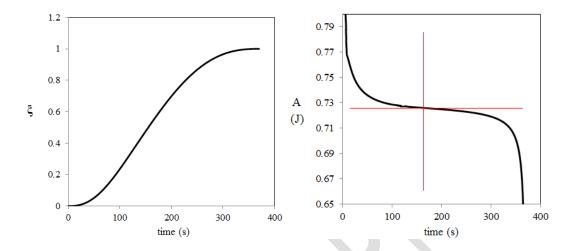


Fig. 5. The extent of process and the affinity versus time for methane hydrate formation at 5.2 MPa.

After calculating the extent of the process and the affinity for the initial stage, the two model parameters can be determined using the logarithmic form of Eq. (3):

$$ln\left(\frac{d\zeta}{dt}\right) = ln\,k + n\,ln\,A\tag{6}$$

The results for the model parameters n and k are presented in Fig. 6 and Table 2. The parameter n was estimated to be approximately -6.8 based on the regression analysis of all experimental data. However, the parameter k did not converge to a constant value and appeared to vary with experimental conditions. As shown in Table 2, k increased by about 10-100 times with rising system pressure and by more than 2-3 orders of magnitude with the addition of THF to the solution. Therefore, k was identified as a kinetic parameter of the model, serving as a criterion for studying the kinetics of hydrate formation.

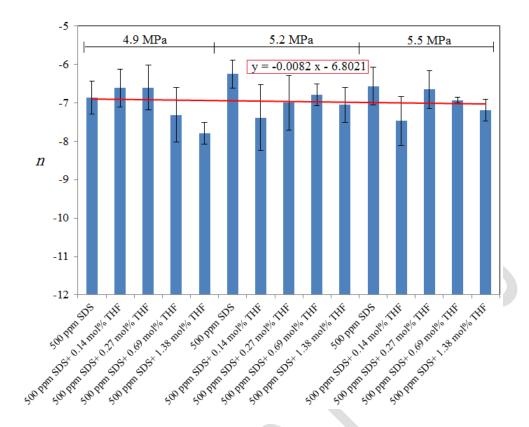


Fig. 6. The model parameter, n, for methane hydrate formation in the presence of SDS and THF.

**Table 2**. The model parameter, k, for methane hydrate formation in the presence of SDS and THF.

P	SDS	THF	k
	(ppm)	(mol%)	
55	500		4.123E-08
		0.14	7.193E-07
		0.27	3.641E-06
		0.69	8.789E-06
		1.38	5.138E-05
52	500		5.115E-09
		0.14	1.241E-08
		0.27	4.529E-08
		0.69	5.346E-08
		1.38	1.271E-07
49	500		1.978E-10
		0.14	4.963E-10
		0.27	1.624E-09
		0.69	4.989E-09
		1.38	1.039E-08

# 3.2. Methane hydrate growth from MD simulation

Fig. 7 displays snapshots of CH<sub>4</sub> hydrate growth during the MD simulation at 240 K and 25 MPa. Over a period of 10 ns, the CH<sub>4</sub> hydrate phase expands, with CH<sub>4</sub> molecules integrating into hydrogen-bonded water molecules

to form stable hydrate clathrates. Fig. 8 shows the time dependence of the number of CH<sub>4</sub> molecules in layers near the hydrate/aqueous phase interfaces, which are about 12 Å thick in the *z*-direction. This data was smoothed by averaging the number of molecules over short segments of the MD trajectory. As evident in Fig. 8, the number of CH<sub>4</sub> molecules near the interfaces increases as the initial gas molecules in the water/CH<sub>4</sub> solution phase rise, which is expected. Additionally, the maximum rate of hydrate growth occurs around 2 ns, with only minor variations afterward.

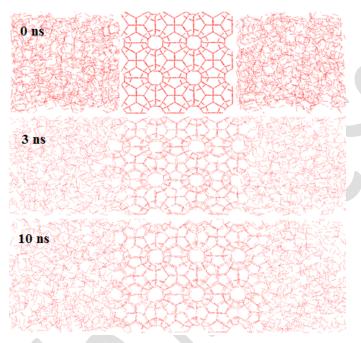


Fig. 7. The snapshots of CH<sub>4</sub> hydrate growth during the simulation at 240 K and 25 MPa with 50 methane molecules in the water/CH<sub>4</sub> solution phase.

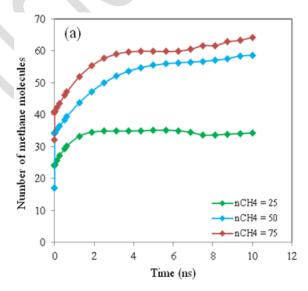


Fig. 8. The number of CH<sub>4</sub> molecules in the layers near the interface as a function of time at 240 K and 25 MPa with the different initial numbers of methane in the water/CH<sub>4</sub> solution phase.

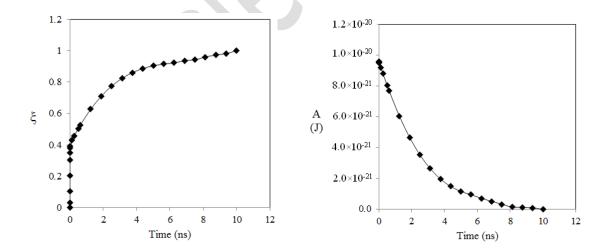
Similar to the process for calculating the model parameters n and k from experimental data, the extent of the process  $\xi$  and the affinity A need to be determined beforehand, as follows:

$$\xi_i = \frac{N_i - N_1}{N_2 - N_1} \tag{7}$$

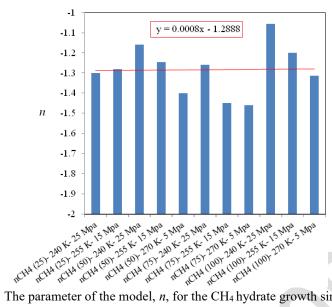
 $N_i$ ,  $N_1$  and  $N_2$  represent the number of methane molecules in the layers around the liquid/solid interfaces at each moment, at the beginning and end of the simulation, respectively. The extent of the process over time for CH<sub>4</sub> hydrate growth is depicted on the left side of Fig. 9. It increases rapidly, approaching an exponential growth rate before stabilizing at nearly zero growth rate, indicating the end of the process. To calculate the affinity, Garfinkle's proposed equation [40] was used:

$$A_i = -RT \ln \sum \xi_i \tag{8}$$

where R is the universal gas constant. As shown in Fig. 9, the affinity reaches its highest value when the hydrate forms. The affinity decreases sharply as the growth process continues and then slows down until equilibrium is reached, consistent with experimental observations. Subsequently, the two model parameters n and k can be determined using the logarithmic correlation of Eq. (6). The results are presented in Fig. 10 and Table 3. The values for n range from -1.46 to -1.05 under different conditions, with an estimated average of about -1.29 based on regression analysis of all simulation data. However, k did not converge to a constant value and was influenced by increasing pressure, showing a rise of more than 2-3 orders of magnitude, and also increased with decreasing temperature. The system pressure and subcooling are proportional to the driving force, leading to faster growth kinetics at higher driving forces. At higher pressures, the interfaces are enriched with gas molecules, and water molecules are more inclined to form methane hydrate clathrates. Lower temperatures increase the solubility of gas molecules in the liquid phase and freeze the molecular motion of water molecules, making the hydrate lattices more rigid due to stronger intermolecular attractive forces. Additionally, an increase in the number of CH<sub>4</sub> molecules in the solution phase can raise the parameter k by about 10 times. It was expected that hydrate formation kinetics would improve as the concentration of CH<sub>4</sub> at the interfaces increased. Thus, k is identified as a kinetic parameter of the proposed model.



**Fig. 9**. The extent of the process and the affinity of hydrate growth versus time at 240 K and 25 MPa with 50 methane molecules in the aqueous solution phase.



**Fig. 10**. The parameter of the model, n, for the CH<sub>4</sub> hydrate growth simulation.

Table 3. The results for the parameter of model, k, at different number of methane in the water/CH<sub>4</sub> solution phase, temperatures and pressures of the system.

<b>n</b> CH4*	T(K)	P (MPa)	k
25	240	25	2.26E-32
	255	15	5.73E-33
50	240	25	8.03E-32
	255	15	6.62E-33
	270	5	1.88E-35
75	240	25	1.31E-31
	255	15	7.31E-32
	270	5	2.38E-35
100	240	25	2.49E-32
	255	15	5.43E-33
	270	5	4.04E-36

The initial number of methane in the water/methane solution phase.

#### 4. Conclusions

In this study, the kinetics of CH<sub>4</sub> hydrate formation were investigated using high-pressure DSC measurements and molecular dynamics (MD) simulations. The kinetic modeling of CH<sub>4</sub> hydrate growth was based on nonequilibrium thermodynamics and the concept of the thermodynamic natural path. This model involves two parameters: one was found to be nearly constant, around -6.8, from experimental data, and between -1.46 and -1.05 from simulation results. The other parameter did not converge to a constant value, varying with different operational conditions, and was identified as a kinetic parameter. The results indicated that this parameter increased by 10-100 times with rising system pressure and by over 2-3 orders of magnitude with the addition of THF. Differences between experimental and simulation results for this parameter may stem from the disparity between macroscopic and microscopic measurement tools.

Overall, this model represents a significant advancement compared to other kinetic models of gas hydrate growth, as it includes at least one parameter that is independent of varying conditions and can be determined both experimentally and theoretically. The proposed model effectively predicts the entire process of gas hydrate growth, as the driving force is not constant: the affinity decreases rapidly at the beginning and then more slowly until it stabilizes, even though the power of the driving force in the kinetic model remains constant.

#### 5. Conclusions

The conclusions may review the main points of the authors' work. Also, it could include the application of the proposed method and suggestions for future research.

#### Nomenclature

A	Affinity
k	Model parameter
n	Model parameter
n <sub>CH4</sub>	Number of methane molecules
P	Pressure
q	Charge
Q	Heat of process
r	Rate of process and Distance vector
R	Universal gas constant
S	Entropy
t	Time
T	Temperature
Greek letters	

#### (

$\sigma$	Cross LJ parameters
$\varepsilon$	Cross LJ parameter
ζ	Extent of process
$\theta$	Angle

# Subscripts

Denoted as irreversible

# **Conflicts of Interest**

The author declares that there is no conflict of interest regarding the publication of this article.

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