

Research Article

Journal of Heat and Mass Transfer Research

Journal homepage[: https://jhmtr.semnan.ac.ir](https://jhmtr.semnan.ac.ir/)

ISSN: [2383-3068](https://portal.issn.org/resource/ISSN/2383-3068)

Chemical Reactions on MHD Couple Stress Fluids towards Stretchable Inclined Cylinder

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1. Introduction

reaction.

Couple stress pertains to the internal forces within a fluid resulting from the distortion of fluid elements. These forces are associated with the swirling motion of fluid particles and can influence the overall fluid behavior. Fluids comprising rigid, randomly dispersed particles within a viscous example being blood, lubricants with minimal polymer additives, electrorheological fluids, and synthetic fluids exhibit such size-dependent effects. Stokes [1] introduced a couple of stresses in viscous fluids, emphasizing the presence of size-dependent effects determined by the material constant and dynamic viscosity, a factor absent in traditional

viscous theories. Rani et al. [2]–[4], Ibrahim, and Gadisa [5]scrutinized the dynamics of couple stress fluid flow around a vertical cylinder. Gajjela and Garvandha [6] delved into the effects of chemical reactions on a couple of stress fluids through a stretching cylinder. Palaiah et al. [7] scrutinized the influence of thermal radiation on magnetized couple stress fluid flowing over a vertical cylinder. Asad et al. [8] investigated heat transfer with variable thermal conductivity in a couple of stress fluids over an inclined stretching cylinder. Khan et al. [9] derived an exact solution for the flow of magnetohydrodynamic (MHD) couple stress fluid. Bharty et al. [10] analyzed the influence of chemical reactions and magnetic fields on the onset of double-diffusive convection

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Cite this article as:

Sharma, S. and Jain, S., 2024. Chemical Reactions on Mhd Couple Stress Fluids towards Stretchable Inclined Cylinder. *Journal of Heat and Mass Transfer Research*, 11(1), pp. 139-150.

within a couple stress fluid confined between elongated parallel plates.

The significance of chemical reactions extends widely across industrial and practical domains. Certain processes involving chemical reactions exhibit a combination of both reactions, such as those found in combustion, biochemical systems, etc. Notably, these reactions can either cease or proceed even without the Occurrence of a catalyst. The interplay between these reactions on catalytic surfaces is remarkably complex, involving varying production and consumption rates within the fluid medium. Many researchers, such as Malik and Khan [11], Rashad et al. [12], Giri et al. [13], and Hayat et al. [14], examined chemical reaction impact over various geometries. Jain and Gupta [15] studied chemical reactions past stretching sheets with suction and injection impacts. Narayana et al. [16] investigated the impact of homogeneousheterogeneous reactions on a couple of stress fluids over a stretching sheet. Naveed et al. [17] investigated the flow of a couple of stress fluids in the grip of chemical reactions past a stretchable sheet. Rana et al. [18] analyzed a couple of stress fluid flows past a Riga plate regarding the effectiveness of chemical reactions. Swapna et al. [19] elucidated the flow of Casson nanofluid in the presence of a chemical reaction coefficient flowing past a linearly stretching surface. Kumari and Jain [20] studied the impact of chemical reactions on Casson fluid. Parmar and Jain [21] investigated chemical reactions past three vertical surfaces.

The study of heat transfer over an inclined stretching surface has garnered attention from numerous researchers due to its diverse applications in industry and technology. This phenomenon is extensively used in wire drawing, fire production, glass fiber manufacturing, and hot rolling processes. Many researchers, Abbas et al. [22], Awan et al. [23], and Sohail and Naz [24], examined the influence of fluid flow and heat transfer over a stretched cylinder. Mabood et al. [25] studied the convective flow of a couple of stress fluids with thermal radiations. Afzal et al. [26] investigated the double-diffusive convection of a couple of stress fluids into a channel. Prasad et al. [27] investigated the flow of couple stress fluid under convective boundary conditions. Mahat et al. [28] studied the mixed convective flow of viscoelastic fluid past a cylinder. Usman et al. [29] observed the heat and mass transfer phenomena in the radiation and activation energy influences on a horizontal porous plate. Fatima et al. [30] investigated the thermal and mass transfer characteristics of viscous fluid flow influenced by buoyancy forces within a channel. Huang et al. [31] investigated mass and heat transfer flow comprising two immiscible fluids

driven by ciliary motion within a channel. Arain et al. [32] examined the bioconvection of nanofluid flowing between parallel plates in the influence of activation energy.

Magnetohydrodynamics (MHD) is essential for a wide array of phenomena, spanning from astrophysical events like solar wind behavior to practical applications such as metal manufacturing, stabilizing fusion processes, refining medical practices like magnetic drug delivery, and enhancing airflow control. Reddy et al. [33] analyzed the impact of heat transfer on MHD fluid flow through a stretching cylinder. Sudarmozhi et al. [34] studied the MHD flow of Maxwell fluid past a stretching cylinder. Hussain et al. [35] analyzed the MHD flow of Williamson fluid with a chemical reaction over a sheet and cylinder. Arain et al. [36] analyzed the flow of Sutterby fluid with the induced magnetic field in the presence of motile gyrotactic microorganisms. Sekhar et al. [37] investigated the dynamic heat and mass transfer on MHD convective flow past an infinitely porous plate.

After reviewing the existing literature, it can be concluded that the characteristics of MHD couple stress fluid with the influence of homogeneous and heterogeneous reactions over an inclined stretching cylinder have not been thoroughly investigated thus far. Consequently, this paper aims to fill this research gap by examining the impact of homogeneous and heterogeneous reactions on a couple of stress fluids past an inclined stretching cylinder in the presence of a porous medium and magnetic field. It is assumed that the diffusion coefficients for species A and B are of similar magnitude. The governing PDEs are evolved and transformed into ODEs using adequate similarity alterations. These ODEs are subsequently solved using the shooting technique in conjunction with the fourth-order Runge-Kutta method, implemented through MATLAB software. The results are presented through graphical representations illustrating the velocity, temperature, and concentration fields.

2. Mathematical Formulation

Consider a two-dimensional flow of steady, incompressible, viscous flow of non-Newtonian fluid with homogeneous–heterogeneous reaction over an inclined stretchable cylinder. This study aims to explore heat transfer analysis under the effect of couple stresses. The *^x* -axis aligns with the cylinder's axis, while the *^r*-axis is normal to it. The cylinder is stretching at a velocity given by $(u(x)) = \frac{0}{x}$ $u_{w}(x) = \frac{U_{0}}{k}$, where U_0 is the reference velocity, and *l* is the characteristic length. The cylinder's inclination is represented by α . A uniform

u v

magnetic field B_0 is also applied along the r direction. The surface maintains constant temperature and concentration, denoted as $T_{\scriptscriptstyle w}$ and *C^w* , respectively. At a distance far from the boundary, these values are represented by $T_{\tiny \infty}$ and $C_{\scriptscriptstyle\omega}$, respectively.

A basic model for reactions, both homogeneous and heterogeneous, within a boundary layer flow was introduced by Chaudhary and Merkin [38]. We consider isothermal cubic autocatalytic kinetic (homogeneous) within the boundary layer flow given by

$$
A + B \to 3B, \text{ rate} = l_1 ab^2 \tag{1}
$$

and single first-order kinetics (heterogeneous) on the catalyst surface as

$$
A \to B, \ \text{rate} = l_s a \tag{2}
$$

here, a and b are concentrations of A and B chemical species and l_1 and l_s are constant. a_0 is the constant concentration of A. The rate of reaction at the outermost edge of the boundary layer will be zero. In the external flow B there is no auto catalyst.

Fig. 1. Diagram for the flow problem

By using these suppositions, the governing equations [Malik et al. (2015)] are as follows:

Continuity equation

$$
\frac{\partial(n)}{\partial x} + \frac{\partial(n)}{\partial r} = 0
$$
 (3)

Momentum equation

 $\frac{\sigma B_0^2}{2}$

 $\mathcal V$ σ $-\frac{v}{k}u - \frac{\sigma B_0^2}{\rho}u$

$$
u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial r} = v \left(\frac{\partial^2 u}{\partial r^2} + \frac{1}{r} \frac{\partial u}{\partial r} \right)
$$

$$
-v' \left(\frac{\partial^4 u}{\partial r^4} + \frac{2}{r} \frac{\partial^3 u}{\partial r^3} - \frac{1}{r^2} \frac{\partial^2 u}{\partial r^2} + \frac{1}{r^3} \frac{\partial u}{\partial r} \right)
$$

$$
+ \left(g \beta_1 (T - T_x) + g \beta_2 (T - T_x)^2 \right) \cos \alpha
$$
 (4)

Energy equation

$$
\frac{\partial T}{\partial x} + v \frac{\partial T}{\partial r} = \frac{k}{\rho c_p} \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right)
$$
(5)

Concentration equation

$$
u \frac{\partial a}{\partial x} + v \frac{\partial a}{\partial r} = D_A \left(\frac{\partial^2 a}{\partial r^2} + \frac{1}{r} \frac{\partial a}{\partial r} \right) - l_1 ab^2
$$

$$
u \frac{\partial b}{\partial x} + v \frac{\partial b}{\partial r} = D_B \left(\frac{\partial^2 b}{\partial r^2} + \frac{1}{r} \frac{\partial b}{\partial r} \right) + l_1 ab^2
$$
 (6)

in which *T* is the fluid temperature, *C* is the fluid concentration, g is gravity, σ is the electrical conductivity, β_1 is thermal expansion coefficient, β_2 is non-linear thermal expansion coefficient, ν is kinematic viscosity, *k* is the thermal conductivity, v' is couple stress viscosity, k' is the permeability of the porous medium, also assuming that both the chemical species *A* and *B* have equal diffusion coefficients $D_{_A}$ and $D_{_B}$.

The pertinent boundary constraints are:

$$
at\ r = R, \ u = u_w(x) = \frac{U_0}{l}x, \ v = V, T \to T_w,
$$

$$
D_A \frac{\partial a}{\partial r} = l_s a, \ D_B \frac{\partial b}{\partial r} = -l_s a
$$

$$
at\ r \to \infty, \ u \to 0, \ \frac{\partial u}{\partial r} \to 0, \ \frac{\partial^2 u}{\partial r^2} \to 0,
$$

$$
T \to T_\infty, \ a \to a_\infty, \ b \to b_\infty
$$
 (7)

Now, we are introducing the similarity transformations [malik et al. (2015)] as follows:

$$
u = \frac{U_0}{l} x f'(\eta), \eta = \frac{r^2 - R^2}{2R} \left(\frac{U_0}{\nu l}\right)^{\frac{1}{2}},
$$

\n
$$
v = -\frac{R}{r} \left(\frac{U_0 V}{l}\right)^{\frac{1}{2}} f(\eta), \theta(\eta) = \frac{T - T_{\infty}}{T_{\infty} - T_0},
$$

\n
$$
m(\eta) = \frac{a}{a_0}, n(\eta) = \frac{b}{a_0}, \text{where, } m(\eta) + n(\eta) = 1.
$$

\n(8)

By employing these dimensionless parameters (8), equations (2-7) are transformed into non-linear ODEs, expressed as follows:

$$
(1+2\gamma\eta)f''' + 2\gamma f'' + ff'' - f'^2
$$

+
$$
(\theta + \gamma_1\theta^2)\lambda \cos\alpha - (d + M)f'
$$

-
$$
K \text{Re}\left[(1+2\gamma\eta)^2 f'''' + 8\gamma(1+2\gamma\eta)f'''' + 8\gamma^2 f'' \right] = 0
$$
 (9)

$$
2\gamma\theta' + (1 + 2\gamma\eta)\theta'' - \Pr(f' \theta - f \theta') = 0
$$
 (10)

$$
(1+2\gamma\eta)m'' + 2\gamma m' + Scfm' - ScLm(1-m)^{2} = 0
$$
 (11)

Reduced appropriate boundary constraints (7) are: $at \ \eta = 0, \ f(0) = -f_w, f'(0) = 1, \ \theta(0) = 1,$ *m* $'(0) = L_s m(0)$ $at \eta \rightarrow \infty$, (12) $f'(\infty) = f''(\infty) = f'''(\infty) = \theta(\infty) \rightarrow 0,$ $m(\infty) = 1$

Where,

$$
L = \frac{l_1 a_0^2 l}{U_0}
$$
 homogeneous reaction
parameter,

$$
L_s = \frac{l_s}{D_A} \sqrt{\frac{vl}{U_0}}
$$

heterogeneous reaction parameter

and the powers denote differentiation concerning η.

The non-dimensional forms of Skin-friction coefficient $C_f = \frac{2v_w}{v}$ 2τ $\sigma_f = \frac{w}{\rho u_w^2}$ $C_f = \frac{2v_w}{\rho u_w^2}$, where $\tau_w = \mu \left(\frac{\partial u}{\partial r} \right)_{r=0}$ $\mathcal{L}_{w} = \mu \left(\frac{\partial u}{\partial r} \right)_{r=R}$ *u* $\left(\frac{u}{r}\right)$, and Nusselt number $=\frac{}{k(T_w-T_w)}$ *w w* $Nu = \frac{xq_w}{k(T - T)}$, where $\begin{pmatrix} x_w \end{pmatrix} = -k \left(\frac{\partial T}{\partial r} \right)_{r=R}$ $q_w = -k \left(\frac{\partial T}{\partial r}\right)$ are $C_f = 2 \text{Re}_x^{-\frac{1}{2}}$ $C_f = 2 \text{Re}_x^2 f''(0)$ and 1 $Nu = -\text{Re}_x^{\frac{1}{2}} \theta'(0)$ respectively, Where $\text{Re} = \frac{U_0 x^2}{vl}$ *l* denotes the local Reynolds number.

3. Method of Solution

The numerical solution for equations (9-11) affected by the boundary conditions (12) has been obtained using the RK-4 method in conjunction with a shooting technique. The chosen method requires a finite domain $0 \leq \eta \leq \eta_{\infty}$ and in this research, a domain of η_{∞} = 10 has been selected.

In the first step, Let

$$
\{f = f_1\}; \{f' = f_2\}; \{f''' = f_3\}; \{f''' = f_4\};
$$

$$
\{f'''' = f_5\}; \{\theta = f_6\}; \{\theta' = f_7\}; \{m = f_8\};
$$

$$
\{m' = f_9\}.
$$

For these assumptions, the non-linear ODEs (9-11) are altered to first-order differential equations in the following form:

$$
f_{4} = \left\{ \frac{1}{K \text{ Re}(1 + 2\gamma\eta)^{2}} \left\{ (1 + 2\gamma\eta) f_{4} + 2\gamma f_{3} - K \text{ Re}\left\{ 8\gamma (1 + 2\gamma\eta) f_{5} + 8\gamma^{2} f_{4} \right\} \right\}
$$

$$
f_{7} = \left\{ \frac{1}{(1 + 2\gamma\eta)} \left\{ \text{Pr}(f_{5}f_{6} - f_{5}f_{7}) - 2\gamma f_{7} \right\} \right\}
$$

$$
f_{9} = \left\{ \frac{1}{(1 + 2\gamma\eta)} \left\{ \text{Pr}(f_{5}f_{6} - f_{5}f_{7}) - 2\gamma f_{7} \right\} \right\}
$$

$$
f_{9} = \left\{ \frac{1}{(1 + 2\gamma\eta)} \left\{ \text{ScL}f_{8} (1 - f_{8})^{2} - 2\gamma f_{8} - \text{Scf}_{5}f_{9} \right\} \right\}
$$

The boundary conditions (12) are reduced as

at
$$
\eta = 0
$$
, $f_1(0) = -f_w$, $f_2(0) = 1$, $f_6(0) = 1$, $f_9(0) = L_s f_8(0)$
at $\eta \to \infty$, $f_2(\infty) = f_3(\infty) = f_4(\infty) = f_6(\infty) \to 0$, $f_8(\infty) = 1$

We guess the values of f_3 , f_7 and f_8 , these are not given at initial conditions. Using step size 0.01, the process is continued, until we get the minimum error term.

4. Results and Discussion

The focus of this paper is to investigate the influence of chemical reactions on MHD couple stress fluid over an inclined stretching cylinder. The numerical solution is obtained using the Runge-Kutta approach with shooting technique. In this section, velocity, thermal, and concentration fields are analyzed against certain relevant parameters. The values of other parameters used to plot the graphs are taken as [Malik et al. [39]] $Pr = 1$, $\gamma = 1$, $K = 1$, $\lambda = 0.1$, $\gamma_1 = 0.1$, $M = 1$, $d = 0.1$, $Sc = 1.6$, $L = 0.1$, $L_{s} = 1.$

We have validated our results with Gajjela and Garvandha [2], for different values of γ and Pr (Table 1).

Figure (2) is plotted to show the velocity field exhibits a decrease as the couple stress parameter increases. This is attributed to the growth of couple stress viscosity with an increasing couple stress parameter, acting as a decelerating force leading to a denser fluid and consequently a reduction in the velocity field.

Figure (3) demonstrates the impact of the curvature parameter on the velocity field. Increasing the curvature parameter, results in a reduction in the cylinder radius, leading to a decrease in the contact area with the cylinder. Consequently, as γ increases, the velocity field near the surface of the cylinder decreases while it enhances farther away from the surface.

Figure (4) demonstrates that mixed convection has the effect of enhancing the velocity profile. As mixed convection grows, the buoyancy force dominates the viscous force that translates the flow from laminar to turbulent, which hastens the fluid flow.

Figure (5) depict the impact of the porosity parameter on the velocity field*.* An escalation in the porosity parameter indicates a greater presence of void spaces or pores within the medium. These empty spaces introduce increased resistance to the fluid flow, causing a decline in velocity. So, the velocity field experiences a decrease with an increase in the porosity parameter (d).

Figure (6) discerns that with an increase in the angle of inclination $(α)$, the velocity field starts to decrease due to a reduction in the gravitational force. This occurrence can be understood by examining the gravitational forces acting both in alignment with and opposing the flow direction. When the angle of inclination is heightened, the effective gravitational force acting in the flow direction diminishes, resulting in a weakening of the force driving the fluid. Consequently, the velocity field, which indicates the speed and direction of fluid flow, undergoes a decline.

Figure (7) presented that the rising value of the magnetic parameter diminishes the velocity profile. Because the magnetic field is directed perpendicular to the cylinder axis, greater values of M amplify the Lorentz force, which, in turn, elevates the fluid's viscosity and subsequently diminishes the velocity distribution.

Figures (8-10) illustrate the impact of different parameters on thermal profiles. Figure (8) depicts the impact of the couple stress parameter on the thermal field. As the parameter of couple stress escalates, the viscosity of couple stress also goes up, causing the fluid to become denser. Consequently, this leads to a rise in the temperature profile.

Figure (9) depicts the impact of the curvature parameter on the thermal profile. As the curvature parameter γ rises, the cylinder radius reduces, causing a reduction in the fluid-cylinder contact area. This, in turn, leads to thicker thermal boundary layers with an increasing curvature parameter γ . Consequently, temperature profiles also rise as γ increases.

Figure (10) demonstrates the impact of the Prandtl number (Pr) on thermal profile. An upsurge in the Prandtl number leads to a reduction in the fluid's thermal diffusivity. The interplay among thermal conductivity, specific heat capacity, and density under constant pressure, termed thermal diffusivity, diminishes with higher Prandtl numbers. A lower thermal diffusivity triggers a decline in heat transfer rate, resulting in a reduction of the thermal boundary layer and, consequently, a decrease in the temperature field.

Fig. 8. Distribution of temperature for *K*

Figures (11-12) shows the concentration profile is enhanced by increasing the value of the homogeneous-heterogeneous reactions parameter. As the homogeneous-heterogeneous reaction parameter rises, it signifies a heightened connection between reactions taking place in the homogeneous phase and those at the heterogeneous interfaces. This increased interaction results in a more complex dispersion of concentrations throughout the system; hence, the concentration profile increases.

Figure (13) is plotted to show the effect of Schmidt number on the concentration field. The Schmidt number quantifies the ratio between momentum diffusivity and mass diffusivity, providing a fundamental insight into the transport properties of a fluid system. Hence, mass diffusivity reduces on rising Schmidt number, which subsides the concentration profile. Figures (14-15) illustrates the variations in the skin friction coefficient and Nusselt number concerning the curvature parameter, mixed convection parameter, and Prandtl number. It is revealed in Figure (14) that the skin friction coefficient experiences an increase with the curvature parameter but decreases with the mixed convection parameter. Conversely, the Nusselt number demonstrates an enhancement for both the curvature parameter and Prandtl number, as observed in Figure (15).

Fig. 15. Skin-friction coefficient for various value of γ and λ

5. Conclusions

A speculative study is done to investigate the influence of homogeneous-heterogeneous reactions on MHD viscous fluid with couple stress over an inclined stretching cylinder in the porous medium. The governing PDEs are evolved and transformed into ODEs by using adequate similarity alterations. These ODEs are subsequently solved using the shooting technique in conjunction with the fourth-order Runge-Kutta approach, implemented through MATLAB software. Then the following results are made:

Table 2. Numerical computation for coefficient of skin friction $f''(0)$; $\theta'(0)$ and $\phi'(0)$ for physical parameters

K	γ	$\mathbf d$	M	Pr	\mathbf{L}	Ls	Sc	$-f''(0)$	$-\theta'(0)$	$-m'(0)$
$\mathbf{1}$								1.25422	1.34860	0.906061
$\boldsymbol{2}$								1.25535	1.34909	0.906062
3								1.25580	1.34925	0.906063
$\overline{4}$								1.25604	1.34932	0.906067
	1.2							1.40092	1.40100	0.88976
	1.4							1.53948	1.45639	0.87399
	1.6							1.67197	1.51387	0.86152
		0.3						1.24949	1.34937	0.906063
		0.5						1.24473	1.35015	0.906066
		0.8						1.23754	1.35132	0.906069
			$\boldsymbol{0}$					1.27739	1.34481	0.906048
			\overline{c}					1.23027	1.35251	0.906073
			3					1.20551	1.35653	0.906085
				$\overline{2}$				1.25209	1.86308	0.906062
				$\mathbf{3}$				1.25113	2.27411	0.906063
				$\overline{4}$				1.25065	2.62086	0.906065
					0.5			1.254217	1.348601	0.90538
					$\mathbf{1}$			1.254219	1.348602	0.89233
					1.5			1.254232	1.348604	0.86405
						0.5		1.25422	1.348606	0.45356
						$\mathbf{1}$		1.25422	1.348606	0.90606
						1.5		1.25421	1.348607	1.35382
							$\overline{2}$	1.254220	1.348608	0.906154
							3	1.254222	1.348612	0.906010
							4	1.254223	1.348615	0.905495

- \triangleright As the couple stress parameter escalates, the velocity profile undergoes a reduction owing to the densification of the fluid, thereby instigating an upward trend in the temperature profile.
- ➢ Elevating the curvature parameter diminishes the contact area with the

cylinder, fostering an enhancement in the velocity profile. Consequently, thicker thermal boundary layers emerge, fostering an augmentation in temperature profiles as γ increases.

 \triangleright A rise in the convection parameter, instigates buoyancy force to overpower viscous force, thereby amplifying the velocity profile.

- \triangleright With the porosity parameter on the rise. the introduction of more void space amplifies the resistance to flow, thereby inducing a decline in the velocity profile.
- \triangleright As the angle of inclination increases, a diminishing gravitational force prompts a decrease in the velocity field.
- ➢ Greater values of M intensify the Lorentz force, thereby augmenting the fluid's viscosity and consequently diminishing the velocity distribution.
- ➢ An escalation in the Prandtl number prompts a reduction in the fluid's thermal diffusivity, leading to a decrease in the heat transfer rate and, subsequently, a decline in the temperature field.
- ➢ The concentration field experiences a decline as homogeneous-heterogeneous reactions intensify, attributable to the heightened dispersion of concentrations across the system, resulting in a more intricate distribution pattern.
- ➢ With a rising Schmidt number, mass diffusivity diminishes, resulting in a subsiding concentration profile.

Nomenclature

- *k* ' Permeability of the porous medium
- L, L Homogeneous, heterogeneous reaction strength
- *l* Characteristic length (m)
- *M* Magnetic field parameter
- Pr Prandtl number
- *Sc* Schmidt number
- *T w* Temperature at surface (K)
- *T* Ambient temperature (K)
- u_{w} Stretching velocity (ms^{-1})
- *V* Velocity of suction/injection

Greek symbols

Funding Statement

This research did not receive any specific grant from funding agencies in the public, commercial, or not-for-profit sectors.

Conflicts of Interest

The author declares that there is no conflict of interest regarding the publication of this article.

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